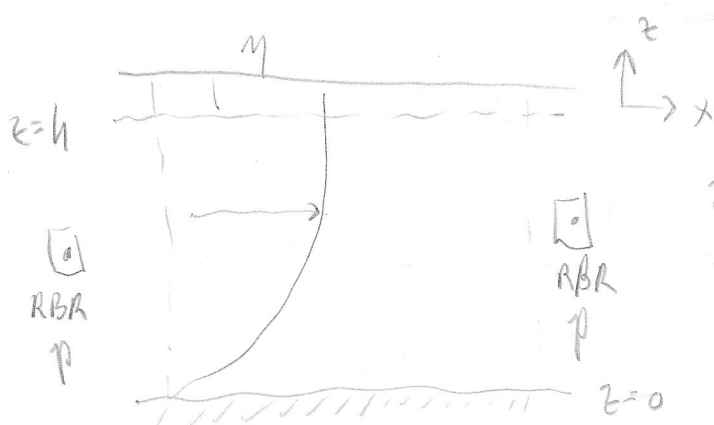


7/23/2019

①

RG

# Unstratified Boundary Layers + Turbulence

Momentum x mm

$$\frac{\partial u}{\partial t} + \underline{u} \cdot \nabla u - f\hat{v} = \underbrace{-\frac{1}{\rho} \frac{\partial p}{\partial x} + \nu \frac{\partial^2 u}{\partial z^2}}_{\text{known cond.}}$$

$$\underbrace{\frac{1}{\rho} \frac{\partial p}{\partial x}}_{mg} = \nu \frac{\partial^2 u}{\partial z^2} \quad \underbrace{mg}_{\checkmark}$$

$$\frac{\partial u}{\partial z} = 0 \quad \text{at } z = h$$

$$u = 0 \quad \text{at } z = 0$$

integrate twice

$$u = \frac{-\frac{1}{\rho} \frac{\partial p}{\partial x}}{\nu} z \left( h - \frac{1}{2} z \right)$$

$$u' = \left( \quad \right) (h - z)$$

$$\frac{1}{\rho} \frac{\partial p}{\partial x} = -1 \times 10^{-4} \text{ m s}^{-2} \quad (1 \text{ cm} / 1 \text{ km})$$

$$\nu = 1 \times 10^{-6} \text{ m}^2/\text{s}$$

$$\Rightarrow U_{\text{surf}} = 5,000 \text{ m/s}$$

∴ it is not laminar flow!

Rewrite x-mom using stress

$$\sigma = -\frac{1}{\rho_0} \frac{\partial p}{\partial x} + \frac{1}{\rho_0} \frac{\partial \tau}{\partial z} \quad \tau = \text{shear stress}$$

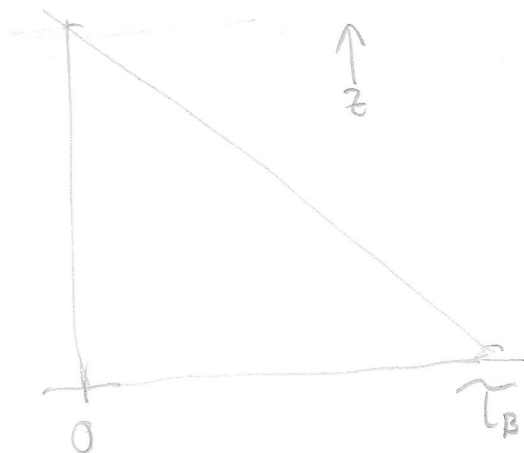
Laminar Flow  $\frac{\tau}{\rho_0} = -\nu \frac{\partial u}{\partial z}$  sign convention?

Turbulent Flow  $\frac{\tau}{\rho_0} = -\langle u'w' \rangle$

so after vertical integral

$$\frac{-1}{\rho_0} \frac{\partial p}{\partial x} = \frac{1}{\rho_0} \frac{\tau_B}{h}$$

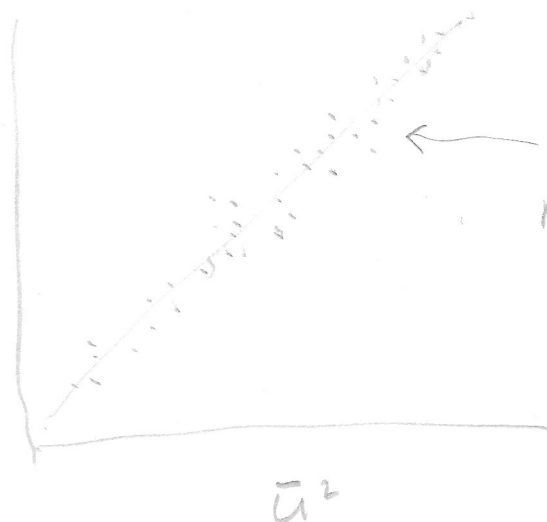
Empirical Evidence



$$\frac{-1}{\rho_0} \frac{\partial p}{\partial x}$$

$$\sim$$

$$\frac{\tau_B}{\rho_0 h}$$



slope =  $C_d$   
 Range  $1.5 - 3.5 \times 10^{-3}$



$\frac{\tau_b}{\rho} \cong C_d U^2$  but to account for changing sign

$\frac{\tau_b}{\rho} \cong C_D \frac{|\bar{u}|}{\bar{u}} \sqrt{\bar{u}^2 + \bar{v}^2}$

coral reef  $C_D \approx 0.1$

North River  
Salt Marsh  $C_D \approx 0.02$

Shallow Estuaries  $C_D = 0.003$

Deep Estuaries  $C_D = 0.002$

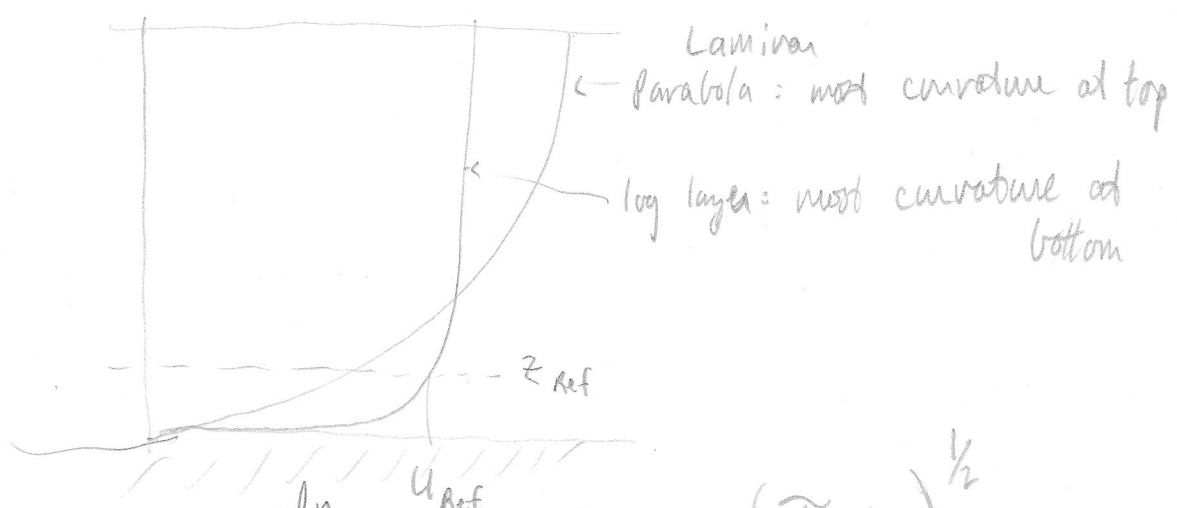
Deep Shelf  
Smooth Bottom  $C_D = 0.001$

Exercise what is stress + bottom pressure  
in your field site [Pa] ?

$\tau = \rho C_d U^2 = 10^3 \cdot 3 \cdot 10^{-3} \cdot 1 = 3 \text{ Pa}$

$p = \rho g h = 10^3 \cdot 10^4 \cdot 10^2 = 10^6 \text{ Pa}$

# The Log Layer



$$u(z) = \frac{u_*}{K} \ln \left( \frac{z}{z_0} \right)$$

$$u_* = \left( \frac{\tau_*}{\rho_0} \right)^{1/2}$$

$K =$  "von Karman's const"  
 $= 0.41$

Nikuradse: sand grain roughness

$z_0 =$  "z naught"  
 Roughness length

$z_0 \approx \frac{1}{30} d_{Nikuradse}$

Also works for sand wave ripple height

Relating  $u_*$  +  $C_D$

$$u_*^2 = C_D \bar{u}^2 = C_{DR} u_{ref}^2 \quad z_{ref} = 1 \text{ m}$$

at a reference height like 1 m

$$u(z_{ref}) = \frac{u_*}{K} \ln \left( \frac{z_{ref}}{z_0} \right) \quad \text{solve for } C_{DR}$$

$$C_{DR} = \left[ \frac{K}{\ln(z_{ref}/z_0)} \right]^2$$

# Relating to Eddy Viscosity

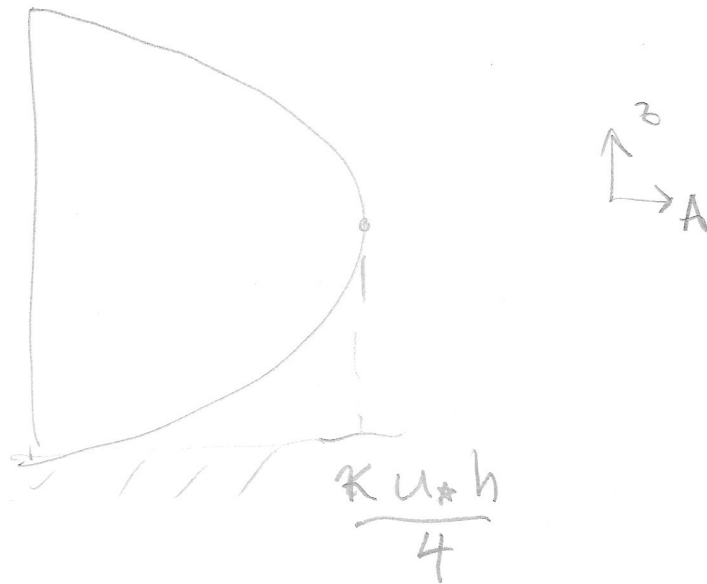
$$A \frac{u_*}{Kz} = \frac{u_*^2}{h} (h-z)$$

(5)

$$\frac{1}{\rho} \frac{\partial p}{\partial x} = \frac{1}{\rho_0} \frac{\partial \tau}{\partial z} = \frac{\partial}{\partial z} \left( A \frac{\partial u}{\partial z} \right) = \frac{\tau_B}{\rho h} = \frac{u_A^2}{h}$$

$$u = \frac{u_*}{K} \log \frac{z}{z_0} \Rightarrow \frac{\partial u}{\partial z} = \frac{u_*}{Kz}$$

$$\Rightarrow A = K u_* z \left( 1 - \frac{z}{h} \right) \quad \text{a parabola}$$



This gives rise to a parabolic velocity profile whereas what actually occurs is a log layer

Homework: compare for  $\frac{1}{\rho_0} \frac{\partial \tau}{\partial x} = 10^{-4} \text{ m s}^{-2}$

$$C_{DL} = 3 \times 10^{-3}, \quad h = 10 \text{ m}$$

$$z_{\text{ref}} = 1 \text{ m}$$